

[of a Minkowski space E] with unit bivector $E = e \wedge e_*$; and

associating a plurality of general homogeneous operators with each data construct to generate a model of the object.

3. The method of claim 1 further comprising:

measuring a scalar distance d_{ab} between two component points a and b encoded as [general] homogeneous points a and b by $d_{ab}^2 = (a - b)^2 = -2a \cdot b$.

4. The method of claim 1 wherein a line through component points a and b encoded as [general] homogeneous points a and b is modeled by $e \wedge a \wedge b$, and a length l_{ab} of a line segment connecting component points a and b is generated by:

$$(l_{ab})^2 = (e \wedge a \wedge b)^2 = (a - b)^2.$$

5. The method of claim 1 wherein a plane through component points a , b , and c encoded as [general] homogeneous points a , b , and c is modeled by $e \wedge a \wedge b \wedge c$, and an area A_{abc} [defined by component points a , b , and c] is generated by $(A_{abc})^2 = \frac{1}{4} (e \wedge a \wedge b \wedge c)^2$.

6. The method of claim 1 wherein a sphere s with radius r centered at a component point c encoded as a [general homogenous radius r and center] homogeneous point c is [generated by] encoded as a vector $s = c + \frac{1}{2}r^2 e$.

7. The method of claim 1 wherein a sphere s determined by four component points a , b , c , d encoded as [general] homogeneous points a, b, c, d is generated by $[s = I E (a \wedge b \wedge c \wedge d)]$, where I is a largest k -blade] $s = (a \wedge b \wedge c)(a \wedge b \wedge c \wedge e)^{-1}$.

8. The method of claim [7 wherein one of the general homogeneous] 1 wherein a plane through component points a, b , and c , d encoded as homogeneous points a, b , and c is [equal to the point e so that s defines a plane through the point e] encoded as a vector $p = I(a \wedge b \wedge c \wedge e) |a \wedge b \wedge c \wedge e|^{-1}$, where I is a unit pseudoscalar.

9. The method of claim [5] 8 wherein a distance[s] between a component homogeneous point a and a component plane p is generated by an inner product[s] $a \cdot p$ of an encoded point a and an encoded plane p].

10. The method of claim 6 wherein a distance[s] between a component homogeneous point a and a component sphere s is [an] generated by an inner product $a \cdot s$ of and encoded point a and the encoded sphere p].

11. The method of claim 6 wherein a distance between two component spheres [s_1 and s_2 encoded as spheres] $s_1 = c_1 + \frac{1}{2}r_1^2 e$ and $s_2 = c_2 + \frac{1}{2}r_2^2 e$ is generated by $\{[s_1 \cdot s_2 = c_1 \cdot c_2 + \frac{1}{2}(r_1^2 + r_2^2) = -\frac{1}{2}[(c_1 - c_2)^2 - (r_1^2 + r_2^2)]]\}$ $s_1 \cdot s_2 = c_1 \cdot c_2 + \frac{1}{2}(r_1^2 + r_2^2)$
 $= \frac{1}{2}[(r_1^2 + r_2^2) - (c_1 - c_2)^2]$.

12. The method of claim 1 wherein the object is a rigid body, and a motion of the rigid body is determined by a time dependent displacement versor $D=D(t)$ satisfying a differential equation $\dot{D} = \frac{1}{2}VD$, with “screw velocity” V given by $V = -I\omega + e\mathbf{v}$, where ω is a velocity and \mathbf{v} is a rotational translational velocity of the rigid body.

13. The method of claim 12 wherein *dynamics* of the rigid body are determined by a differential equation $\dot{P} = W$, where $P = -I\mathbf{L} + e_*\mathbf{p}$, and $W = -I\mathbf{T} + e_*\mathbf{F}$, where \mathbf{L}

is an angular momentum and \mathbf{p} is a translational momentum of the rigid body, while \mathbf{T} is [the] a net torque and \mathbf{F} is a net force on the rigid body.

14. The method[s] of claim 12 wherein the [rigid body includes] object is composed of n linked rigid components, and a motion of the [rigid body] object is modeled by n time dependent displacement versors D_1, D_2, \dots, D_n , [and] with a motion of a k^{th} linked rigid component [is] determined by a versor product $D_1 D_2 \dots D_k$.

15. The method of claim 1 wherein the object[s] is a robot composed of a plurality of [links] rigid bodies connected at joints.

Amended Claims

1. A method for modeling an object composed of one or more components, comprising:

inputting data for each component of the object, the data including coordinates expressed in Euclidean space for a plurality of points \mathbf{x} of each component;

encoding each point \mathbf{x} as a null vector x in a homogeneous space by $x = (\mathbf{x} + \frac{1}{2}\mathbf{x}^2 e + e_*)E = \mathbf{x}E - \frac{1}{2}\mathbf{x}^2 e + e_*$, where e and e_* are null vectors with unit bivector $E = e \wedge e_*$; and

associating a plurality of general homogeneous operators with each data construct to generate a model of the object.

3. The method of claim 1 further comprising:

measuring a scalar distance \mathbf{d}_{ab} between two component points \mathbf{a} and \mathbf{b}

encoded as homogeneous points a and b by $\mathbf{d}_{ab}^2 = (a - b)^2 = -2a \bullet b$.

4. The method of claim 1 wherein a line through component points \mathbf{a} and \mathbf{b} encoded as homogeneous points a and b is modeled by $e \wedge a \wedge b$, and a length \mathbf{l}_{ab} of a line segment connecting component points \mathbf{a} and \mathbf{b} is generated by:

$$(\mathbf{l}_{ab})^2 = (e \wedge a \wedge b)^2 = (a - b)^2.$$

5. The method of claim 1 wherein a plane through component points \mathbf{a} , \mathbf{b} , and \mathbf{c} encoded as homogeneous points a , b , and c is modeled by

$e \wedge a \wedge b \wedge c$, and an area A_{abc} is generated by $(A_{abc})^2 = \frac{1}{4} (e \wedge a \wedge b \wedge c)^2$.

6. The method of claim 1 wherein a sphere \mathbf{s} with radius \mathbf{r} centered at a component point \mathbf{c} encoded as a homogeneous point c is encoded as a vector $\mathbf{s} = c + \frac{1}{2}r^2e$.

7. The method of claim 1 wherein a sphere \mathbf{s} determined by four component points \mathbf{a} , \mathbf{b} , \mathbf{c} , \mathbf{d} encoded as homogeneous points a, b, c, d is generated by $\mathbf{s} = (a \wedge b \wedge c)(a \wedge b \wedge c \wedge e)^{-1}$.

8. The method of claim 1 wherein a plane through component points a, b , and c encoded as homogeneous points a , b , and c is encoded as a vector $\mathbf{p} = I(a \wedge b \wedge c \wedge e) |a \wedge b \wedge c \wedge e|^{-1}$, where I is a unit pseudoscalar.

9. The method of claim 8 wherein a distance between a component homogeneous point \mathbf{a} and a component plane \mathbf{p} is generated by an inner product $\mathbf{a} \bullet \mathbf{p}$.

10. The method of claim 6 wherein a distance between a component homogeneous point \mathbf{a} and a component sphere \mathbf{s} is generated by an inner product $\mathbf{a} \bullet \mathbf{s}$.

11. The method of claim 6 wherein a distance between two component spheres $s_1 = c_1 + \frac{1}{2}r_1^2 e$ and $s_2 = c_2 + \frac{1}{2}r_2^2 e$ is generated by $s_1 \bullet s_2 = c_1 \bullet c_2 + \frac{1}{2}(r_1^2 + r_2^2) = \frac{1}{2}[(r_1^2 + r_2^2) - (c_1 - c_2)^2]$.

12. The method of claim 1 wherein the object is a rigid body, and a motion of the rigid body is determined by a time dependent displacement versor $D=D(t)$ satisfying a differential equation $\dot{D} = \frac{1}{2}VD$, with “screw velocity” V given by $V = -I\omega + e\mathbf{v}$, where ω is a velocity and \mathbf{v} is a rotational translational velocity of the rigid body.

13. The method of claim 12 wherein *dynamics* of the rigid body are determined by a differential equation $\dot{P} = W$, where $P = -I\mathbf{L} + e_*\mathbf{p}$, and $W = -I\mathbf{T} + e_*\mathbf{F}$, where \mathbf{L} is an angular momentum and \mathbf{p} is a translational momentum of the rigid body, while \mathbf{T} is a net torque and \mathbf{F} is a net force on the rigid body.

14. The method of claim 12 wherein the object is composed of n linked rigid components, and a motion of the object is modeled by n time dependent displacement versors D_1, D_2, \dots, D_n , with a motion of a k^{th} linked rigid component determined by a versor product $D_1 D_2 \dots D_k$.

15. The method of claim 1 wherein the object is a robot composed of a plurality of rigid bodies connected at joints.